

# TS 4001: Lecture Summary 5

## Powering

# Powering

- Resistance is only the means to get to power.
- The real question is:
  - How fast can the ship go?
  - How much power to install for a required speed?

# First Relationships

- $(\text{Power}) = (\text{Force}) \times (\text{Speed})$
- $(\text{Force}) \sim (\text{Resistance})$
- $(\text{Resistance}) \sim (\text{Speed})^2 \times (\text{Wetted Surface})$
- $(\text{Wetted Surface}) \sim (\text{Volume})^{2/3} \text{ or } (\text{Displacement})^{2/3}$
- Therefore:
  - $(\text{Power}) = (\text{Coefficient}) \times (\text{Speed})^3 \times (\text{Displacement})^{2/3}$
  - This (Coefficient) is known as the “Admiralty Coefficient”

# Initial Powering Estimates

- Parametric data most appropriate for concept designs

- Scaled power from similar ships

$$SHP_2 = SHP_1 \left( \frac{V_2}{V_1} \right)^3 \left( \frac{\Delta_2}{\Delta_1} \right)^{\frac{2}{3}} \left( \frac{PC_1}{PC_2} \right)$$

- Regression analysis of similar ships

- Standard series methods

- More accurate analysis which requires more detailed information
- Frictional resistance based on ITTC-57 or other friction line
- Residuary resistance from Taylor, Series-64, SSPA, or NPL series
- Many codes exist for these predictions

- Estimated propulsive coefficients

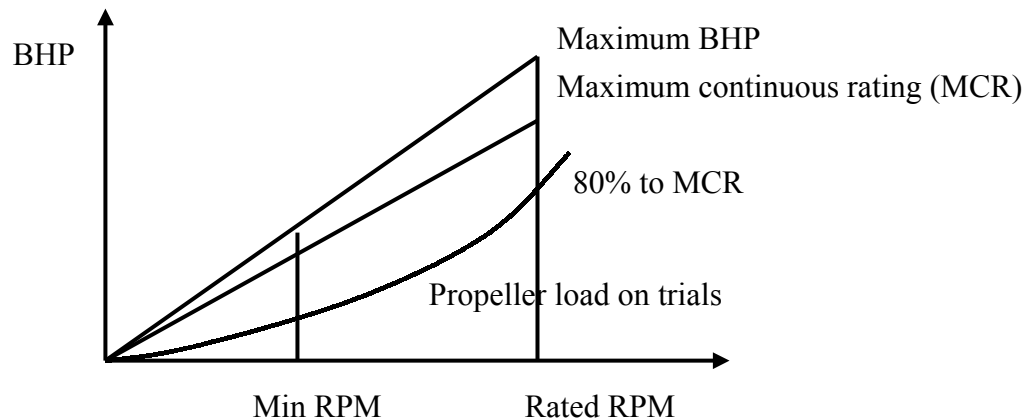
- Regression analysis for PC,  $\eta_o$ , wake fraction, and thrust deduction
- Educated guess for transmission, shafting, and  $\eta_P$

# Powering Estimates

- Method of Admiralty Coefficient works well for similar designs.
- Methods such as Silverleaf & Dawson and Holtrop are based on parametric equations and a large regression analysis.
- Estimation of power through systematic series:
  - Estimation of effective power and propeller performance separately.
  - Use the ITTC line for frictional resistance.
  - Estimate or calculate the hull wetted surface.
  - Estimate the residuary resistance through Taylor series, Series 60, etc.
  - Estimate the propeller efficiency through regression analysis or propeller charts.
  - Estimate wake fraction, thrust deduction factor, and relative rotative efficiency from regression formulas.

# Powering Margins

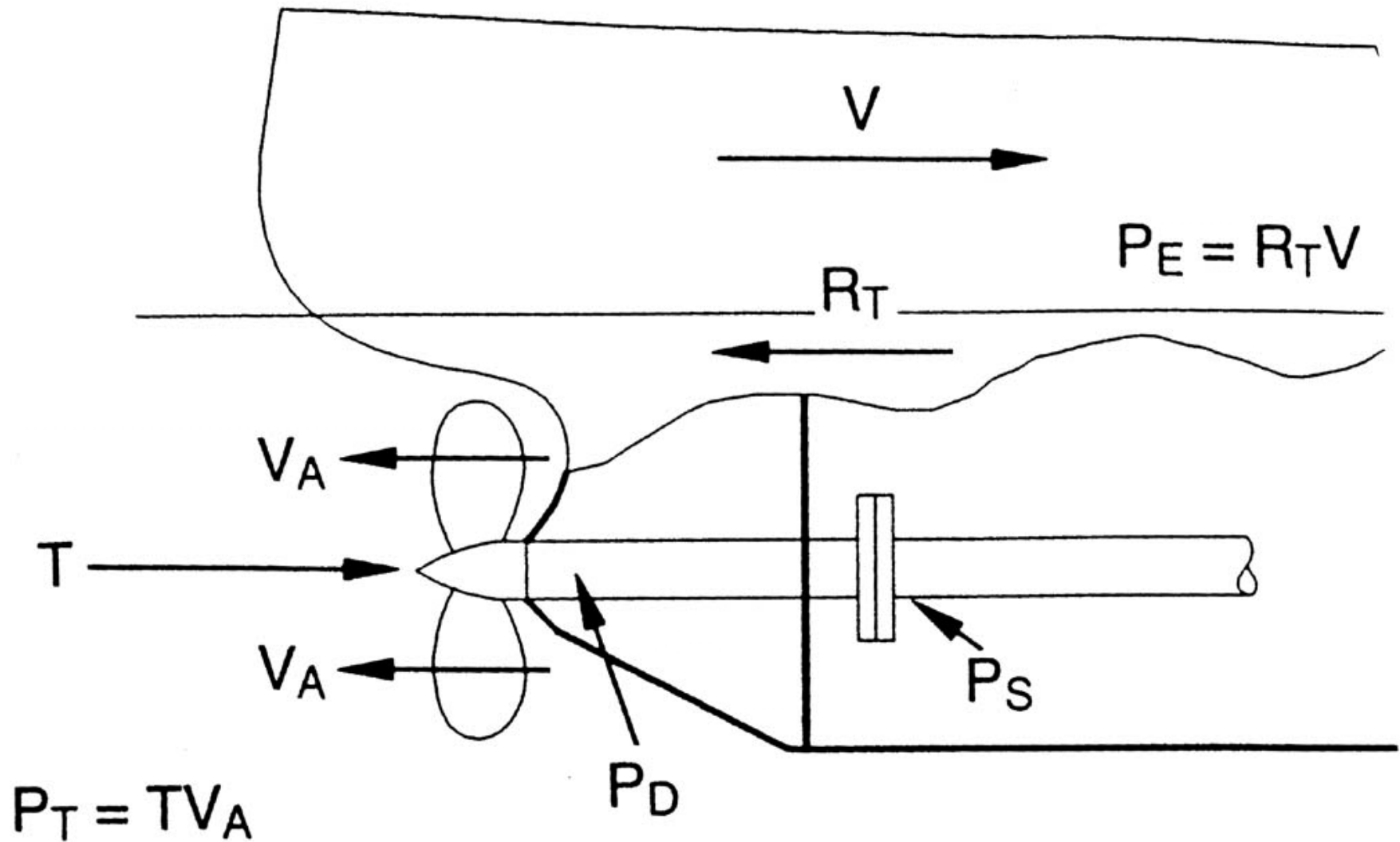
- Design margin:
  - 10% Very early predictions before body plan and appendage configuration
  - 8% Preliminary design predictions made prior to model tests
  - 6% Preliminary and contract design after SHP test with stock propeller with corrections for expected propeller
  - 2% Contract design after SHP test with actual propeller design
- Service margin:
  - To allow for sea conditions, hull and propeller fouling, etc.
  - Typically 10 to 20% below MCR.



# Powering Software

- Use similar designs
- Spreadsheet models
- Warship-21
- PPP
- ASSET
- AUTOHYDRO

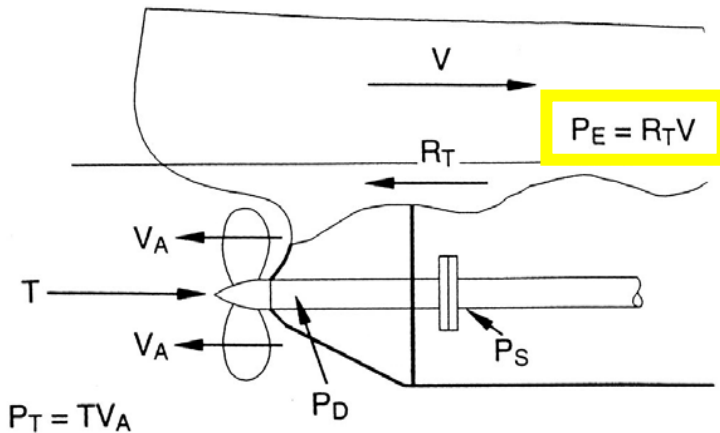
# Definitions





# Effective Power, EHP

- $P_E$  or EHP = power needed to tow ship at a given speed in calm water or power to overcome total resistance force  $R_T$  at ship speed  $V$ .
- $P_E = R_T V$ , where  $R_T$  = total resistance and  $V$  = speed.
- Can be evaluated straight following resistance calculations.

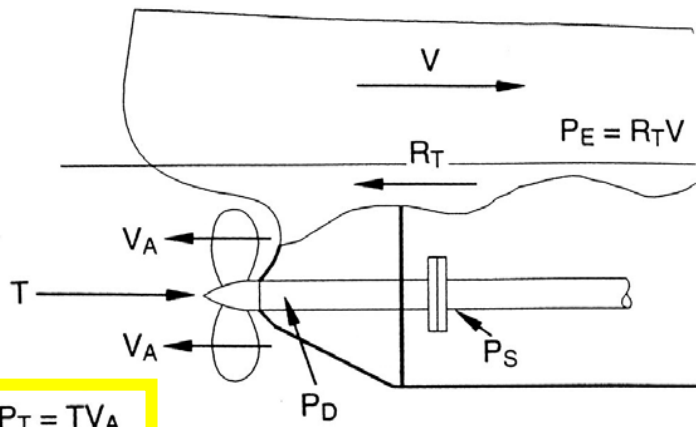


$$EHP = \frac{R_T V}{550} \text{ where } R_T \text{ [lbs], } V \text{ [ft/sec]}$$

$$EHP = \frac{R_T V_K}{325.6} \text{ where } R_T \text{ [lbs], } V \text{ [knots]}$$

# Thrust Power, THP

- Propeller is producing thrust,  $T$  at a speed of advance,  $V_A$ .
- Useful power output of the propeller is called the Thrust Power,  $P_T$  or THP.



$$P_T = T V_A$$

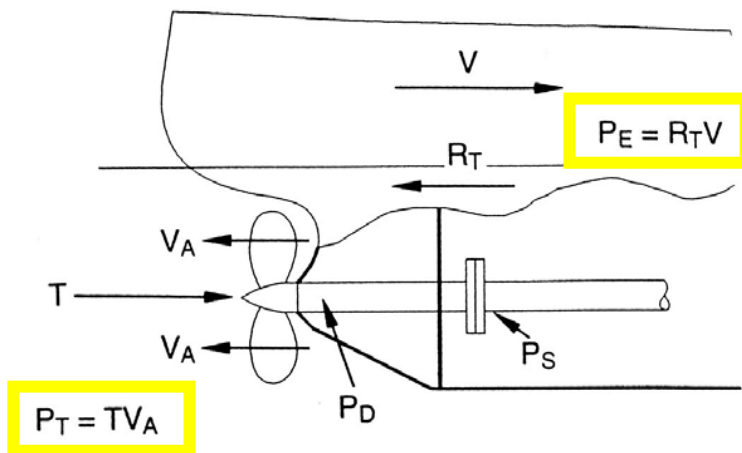
$$T \neq R_T$$

$$V_A \neq V$$

# Hull Efficiency

$$\text{Hull efficiency } \eta_H = \frac{P_E}{P_T} = \frac{R_T V}{T V_A}$$

A measure of hull (stern) design to suit propulsor arrangement.



- It does not involve power conversion, so it is not a “true” efficiency.
- It can be greater than one, usual numbers around 1.05.

- 
- The diagram illustrates a closed-loop system with a pump and a turbine. The pump, on the left, has an inlet labeled  $T$  and an outlet labeled  $V_A$ . The pressure at the pump outlet is given by  $P_T = TV_A$ . The turbine, on the right, has an inlet labeled  $P_S$  and an outlet labeled  $R_T$ . The pressure at the turbine inlet is  $P_D$ , which is highlighted in a yellow box. The system flow is indicated by  $V$  and  $P_E = R_TV$ .

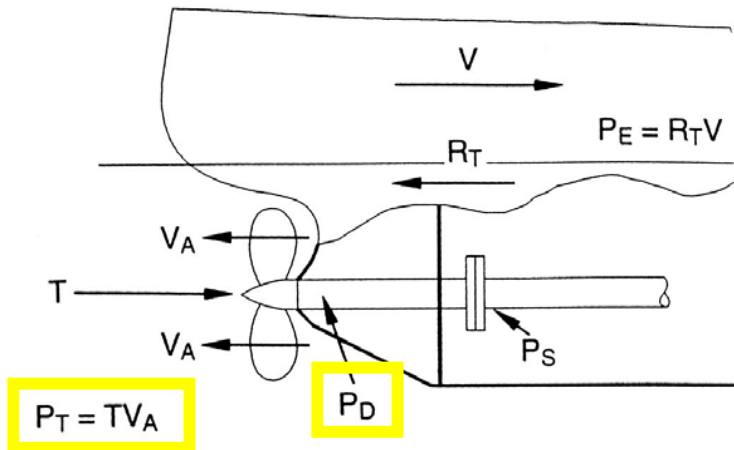
$n$  = Revolutions per second of shaft/propeller.  
 $Q_D$  = Torque delivered to the propeller.

# Propeller Efficiency

- Power conversion between  $P_D$  and  $P_T$  is where the major loss is.
- Depending on where torque is measured:
  - Efficiency of propeller behind the ship,  $\eta_B$ .
  - Efficiency of propeller in open water,  $\eta_0$ .

$$\eta_B = \frac{P_T}{P_D} = \frac{TV_A}{2\pi nQ_D}$$

$$\eta_0 = \frac{TV_A}{2\pi nQ_0}$$



$Q_D$  = Torque required by the propeller to deliver  $T$  at  $V_A$  **behind the ship**.

$Q_0$  = Torque required by the propeller to deliver  $T$  at  $V_A$  **in open water**.

# Relative Rotative Efficiency

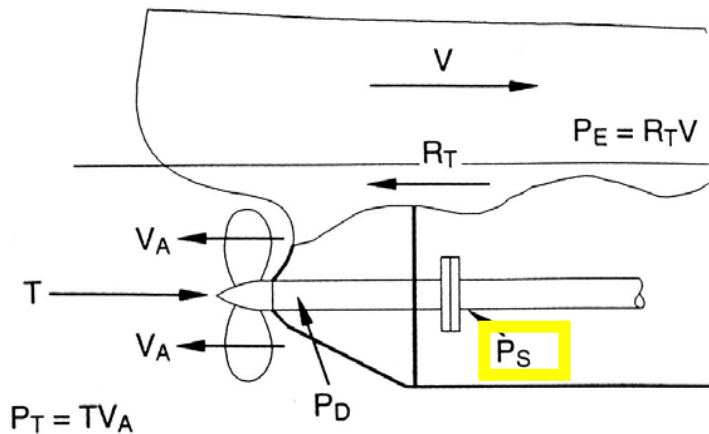
- Defined by the ratio:

$$\eta_R = \frac{\eta_B}{\eta_0} = \frac{Q_0}{Q_D}$$

- It is not a “true” efficiency (not a ratio of powers).
- It can be greater than one.
- Usual values around one.

# Shaft Power, SHP

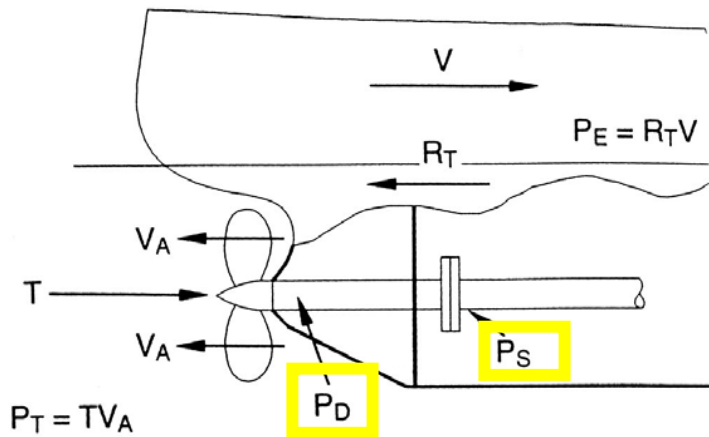
- Power output at the prime mover is higher than delivered power.
- It is usually called shaft power ( $P_S$  or SHP) for gas turbines and brake power ( $P_B$  or BHP) for diesel engines.



- Occasionally,  $P_S$  is the power immediately fore of the stern tube bearing, and  $P_B$  is the power right at the prime mover.

# Transmission Efficiency

$$\text{Shaft transmission efficiency, } \eta_s = \frac{P_D}{P_S}$$

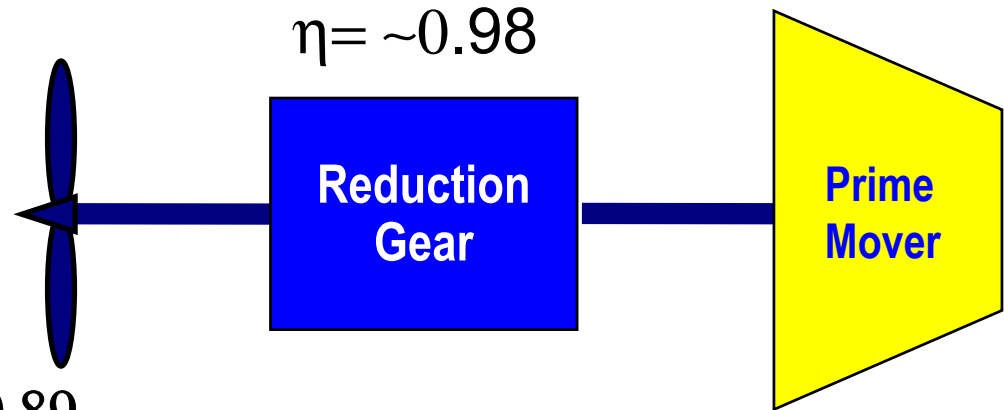


- Occasionally, more than one transmission (or mechanical) efficiencies are defined.
- The overall transmission efficiency will then be the product of the individual components.

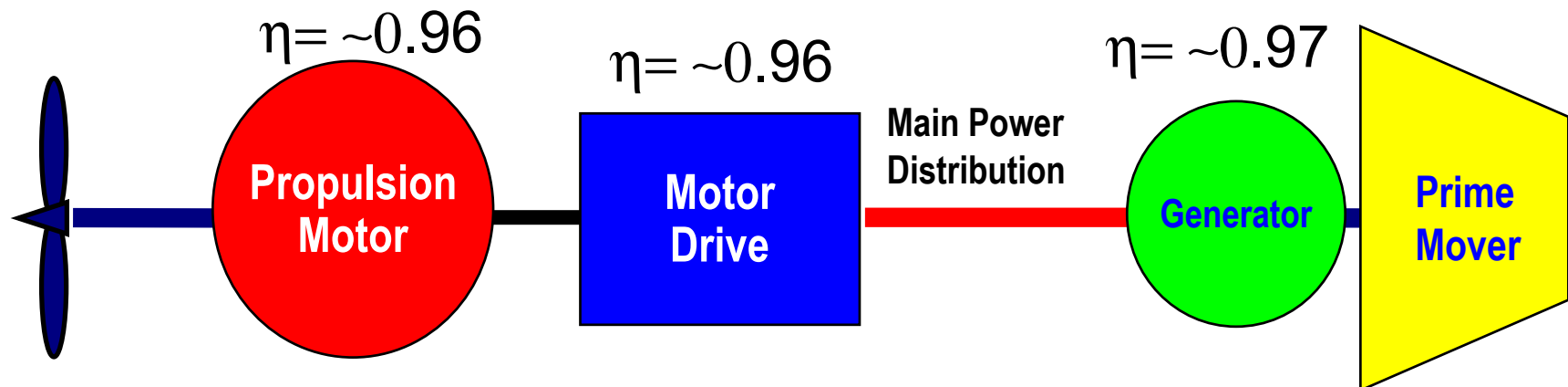


# Transmissions

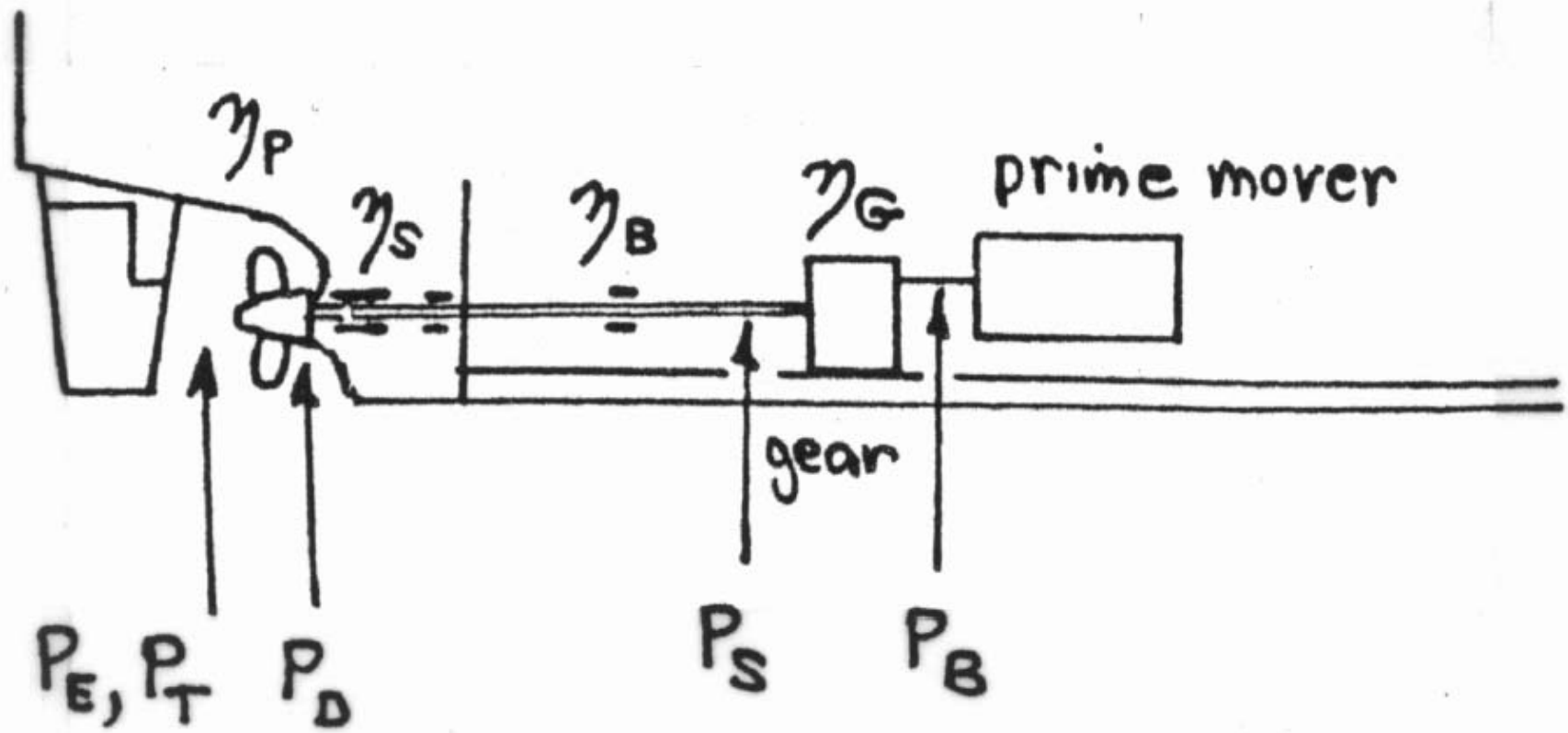
- Geared Drives



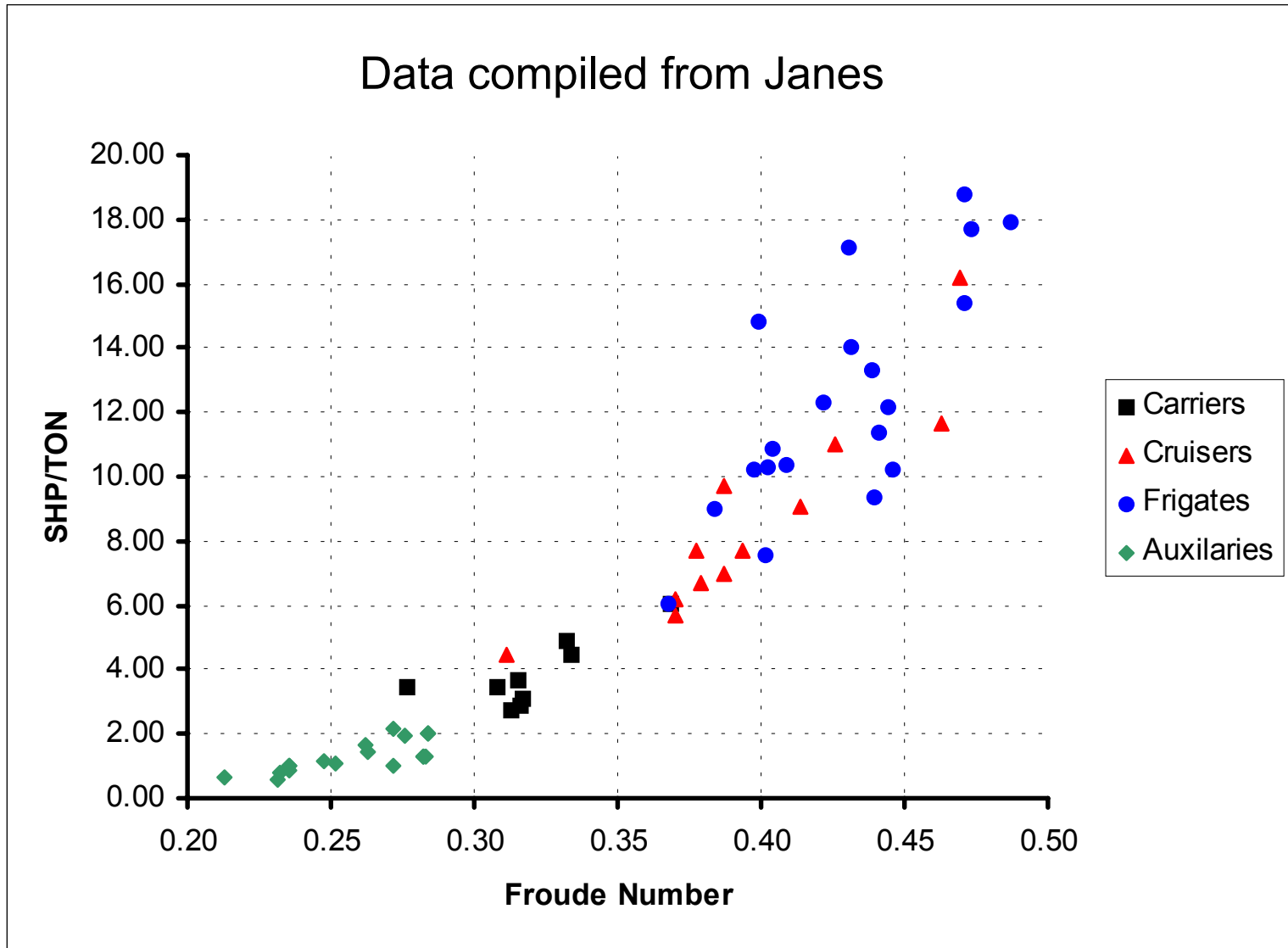
- Electric Drives  $\eta_{tr} = \sim 0.89$



# Summary



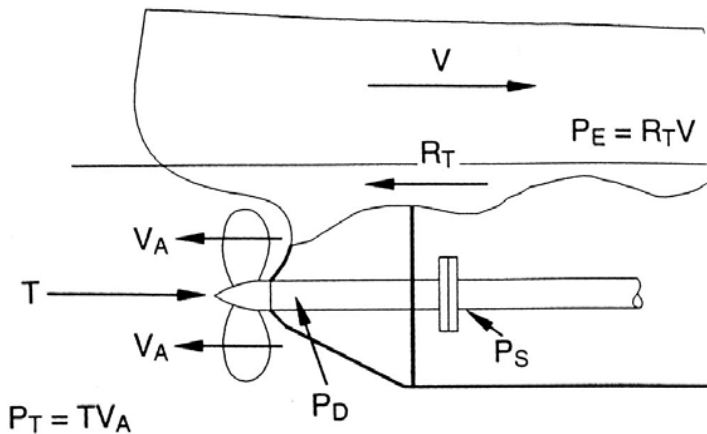
# Speed-Power Trends



# Overall Efficiency

Overall Efficiency, also known as Propulsive Efficiency,  
or Propulsive Coefficient (PC) is

$$\eta_P = \frac{P_E}{P_S} = \frac{P_E}{P_T} \times \frac{P_T}{P_D} \times \frac{P_D}{P_S} = \eta_H \eta_B \eta_S = \eta_H \eta_0 \eta_R \eta_S$$



$\eta_H$ ,  $\eta_0$ ,  $\eta_R$  depend on hydrodynamics.

$\eta_S$  depends on mechanical efficiencies.

$\eta_0$  is where the major loss is.

**The Powering Problem: Maximize  $\eta_P$**

Will do this after we see how propellers work.

# Endurance Fuel Estimation

- For Navy designs, use NAVSEA Design Data Sheet (DDS) 200-1
- Standard procedure for calculation based on:
  - Range
  - Cruise speed
  - Required SHP
  - Engine loading
  - Transmission efficiency
  - 24-Hour electric load
  - SFC
  - Margins and allowances
- Second step is to calculate volume required for fuel tankage by multiplying fuel weight in LT by 47.4

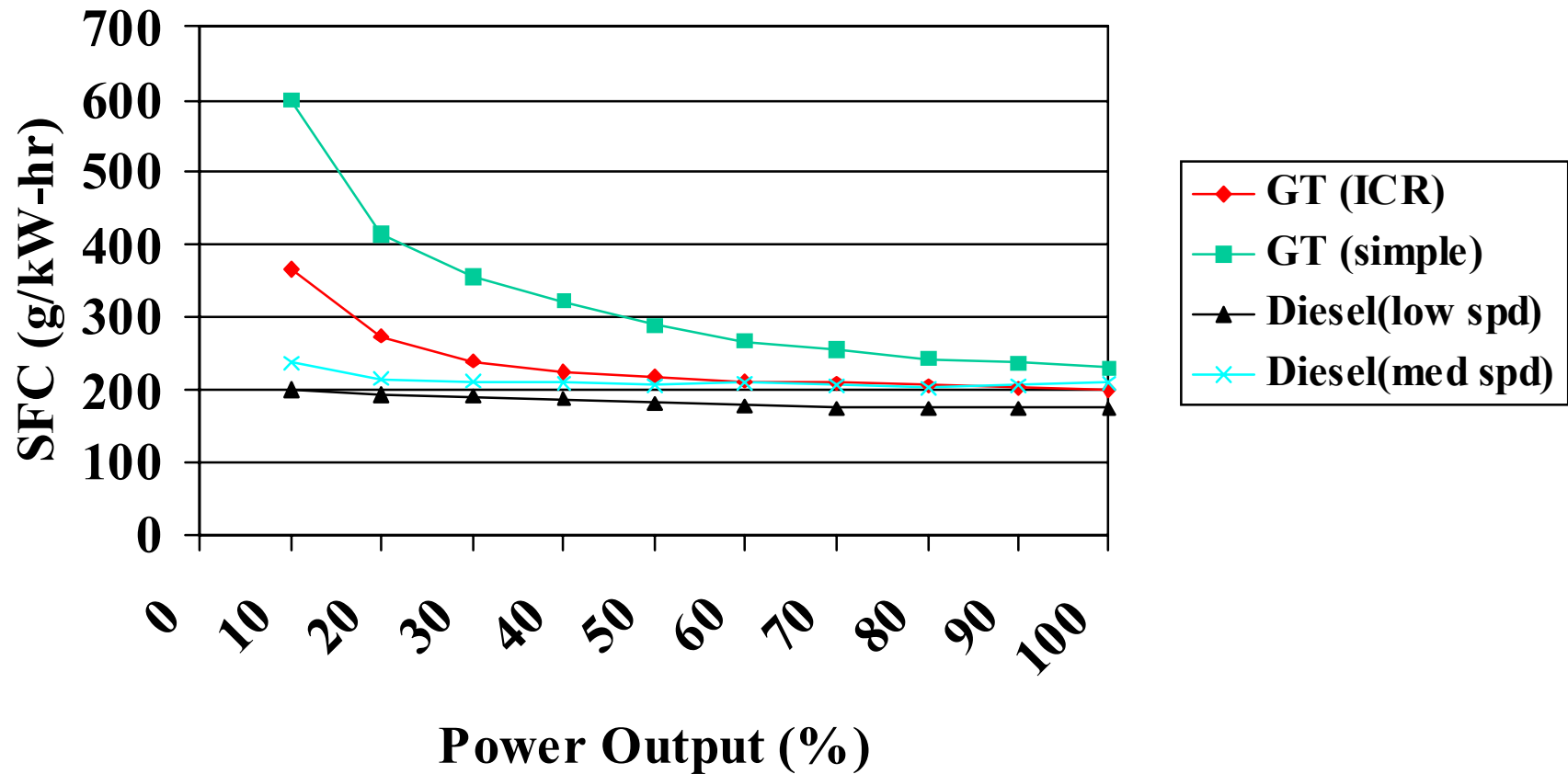
# Calculations

NO.	ITEM	UNITS	SOURCE
1	Endurance Required	NM	Given
2	Endurance Speed	KNOTS	Given
3	Full Load Displacement	LTONS	Given
4	Rated Full Power	HP	Given
5	Design Endurance Power @ (2) & (3)	HP	Given
6	Average Endurance Power	HP	(5) * 1.10
7	Average Endurance Power/Rated Full Power		(6) / (4)
8	Average Endurance BHP	HP	(6) / Trans. Eff.
9	24-hour Average Electric Load	kW	Given
10	Propulsion Fuel Rate @ (8)	lb/SHP/hr	Given
11	Propulsion Fuel Consumption	lb/hr	(10) * (8)
12	Generator Fuel Rate @ (9)	lb/hr	Given
13	Generator Fuel Consumption	lb/hr	(12) * (9)
14	Fuel Consumption for Other Services	lb/hr	Given
15	Total All-Purpose Fuel Consumption	lb/hr	(11) + (13) + (14)
16	All-Purpose Fuel Rate	lb/SHP/hr	(15) / (6)
17	Fuel Rate Correction Factor Based on (7)		Given
18	Specified Fuel Rate	lb/SHP/hr	(16) * (17)
19	Average Endurance Fuel Rate	lb/SHP/hr	(18) * 1.05
20	Endurance Fuel	LTONS	(1)*(6)*(19)/(2)/2240
21	Safety Factor		Given
22	<b>Endurance Fuel Load</b>	<b>LTONS</b>	<b>(20) / (21)</b>

# Impact of Fuel on Ship System

- Range and cruise speed have significant impact on ship size and cost
- Every ton of fuel is one less ton of payload the ship can carry
- For every ton of fuel, ships must now have tankage for one ton of ballast
- If tankage volume exceeds that available in otherwise non-arrangeable areas of the ship, the ship must grow to accommodate the extra fuel
- As required tankage volume increases, the center of gravity of the fuel rises, causing the overall ship KG to rise
- Increased fuel requirement impacts the fuel oil transfer and service systems
- In addition to increased acquisition cost due to extra weight and volume, fuel costs greatly impact annual O&S costs

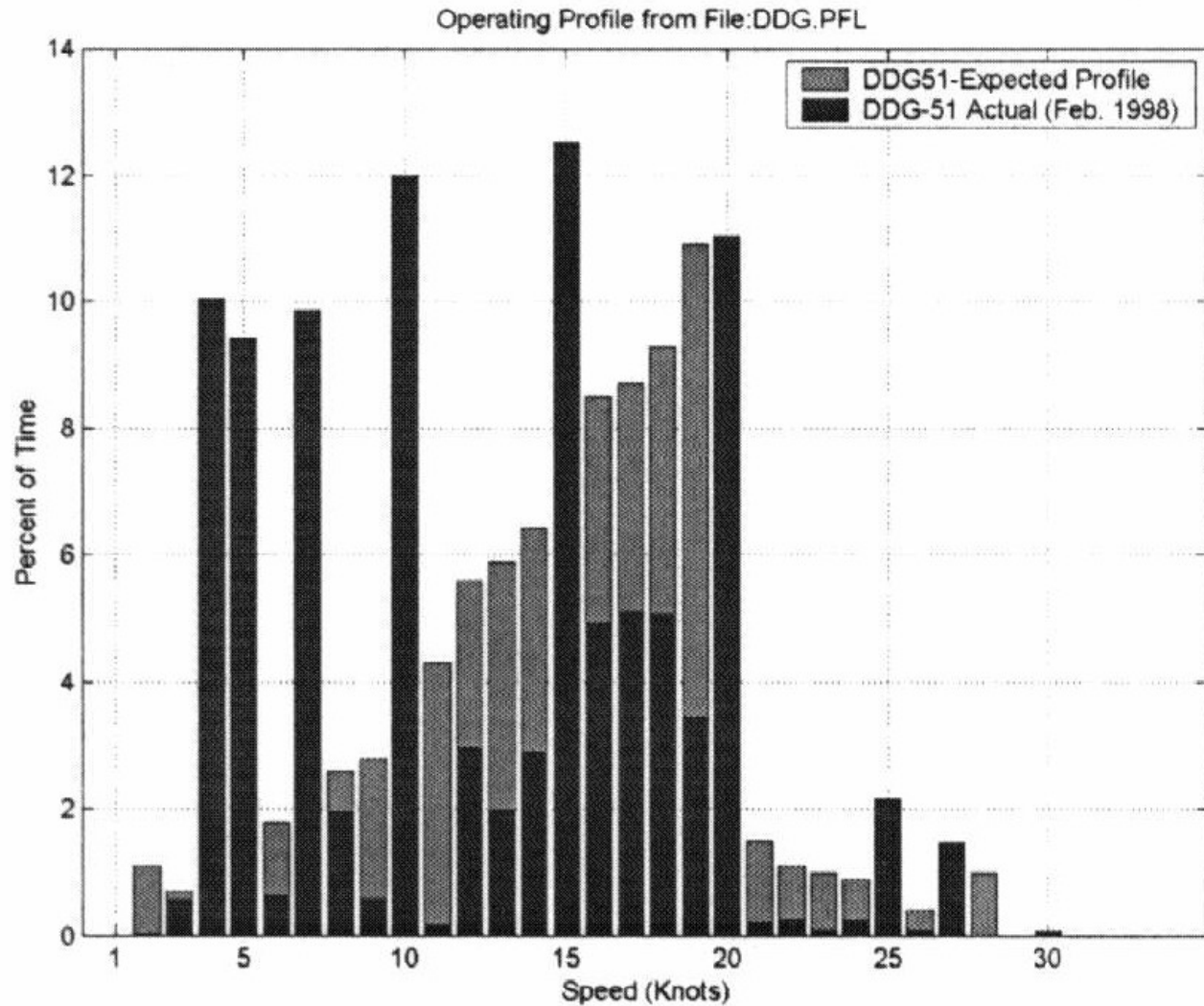
# SFC Comparison





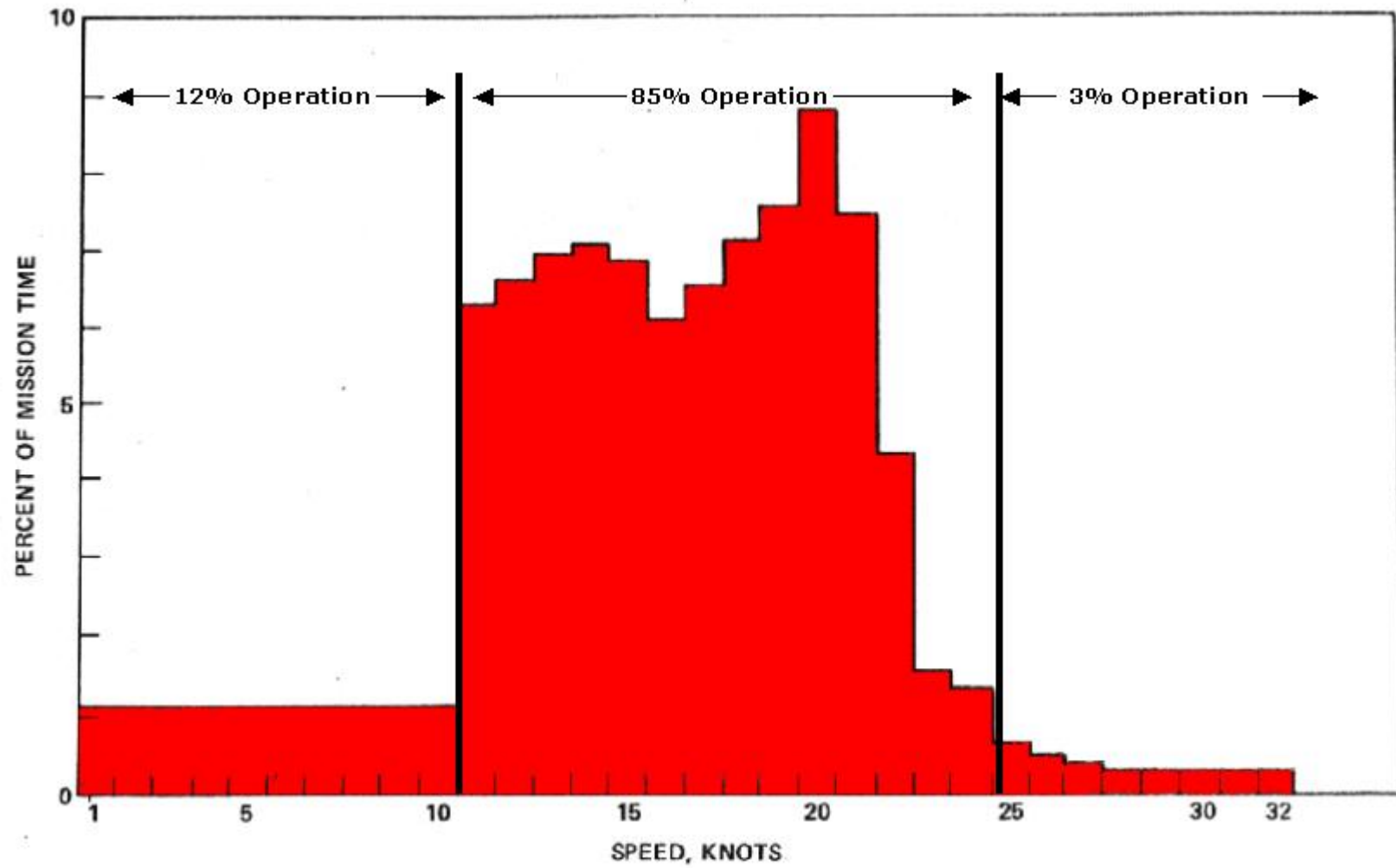
# Speed Operational Profile

When comparing power plants take into account the ship's operational profile.





# A Typical Profile

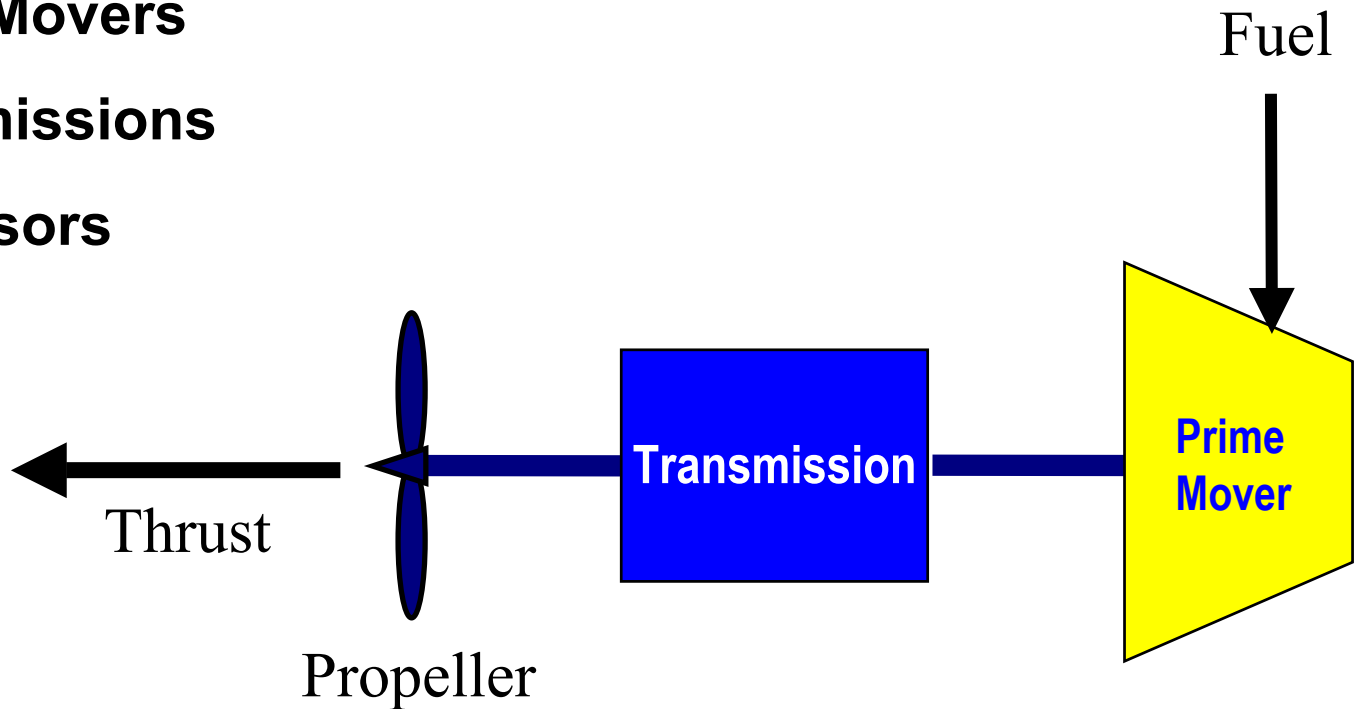


Standard Destroyer Mission Profile

# Propulsion Plant

- **Subsystems / Components**

- Prime Movers
- Transmissions
- Propulsors



# Prime Movers

- Diesels
- Gas Turbines
  - Simple cycle
  - ICR
- Steam
  - Conventional
  - Nuclear
- Fuel Cells
- Combinations

# Additional Reading

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- 1.4.1 Ship Resistance and Propulsion Notes.
- 1.5.1 The Use of Stern Flap Technology (M. Zoccola).